

12/2 ①

* HW will be due Friday, 1 additional problem

Midterm Statistics:

mean : 82

median : 87

The Linear Quadratic Regulator (LQR)

* An "optimally designed" state feedback gain matrix K

For us:

- ① specify a good performance criterion, ~~and~~ ~~and~~ in terms of closed loop response
- ② LQR algorithm returns optimal K

Mathematical Setup of LQR problem ⁽²⁾

System Dynamics $\dot{x} = Ax + Bu$

$\uparrow$
control
input

Problem: Design K , so that

$$u(t) = K x(t)$$

Performance Objective

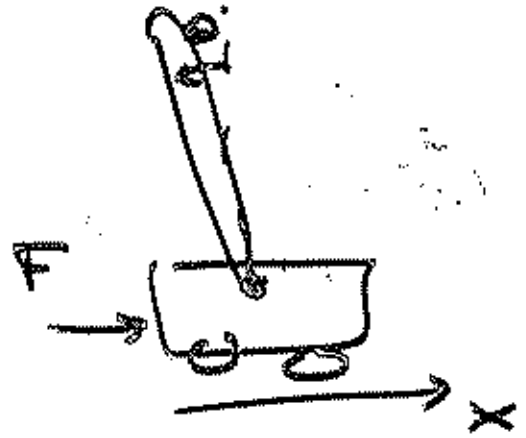
$$J = \int_0^{\infty} \left[\underbrace{x^T(t) Q x(t)}_{\text{quadratic function of } x} + \underbrace{u(t) R u(t)}_{\text{quadratic function of } u} \right] dt$$

LQR: given A, B, Q, R

produce K that gives the smallest possible objective J

Meaning of quadratic objectives: (3)

Ex: Inverted Pendulum

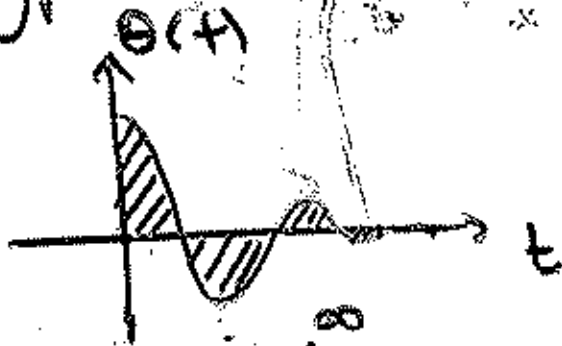


$$\frac{d}{dt} \begin{bmatrix} \theta \\ \dot{\theta} \\ x \\ \dot{x} \end{bmatrix} = \begin{bmatrix} A \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \\ x \\ \dot{x} \end{bmatrix} + \begin{bmatrix} B \end{bmatrix} F$$

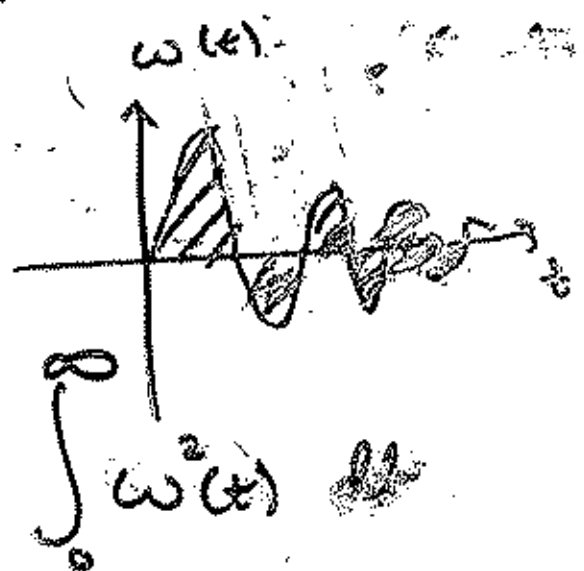
state
feedback

$$F(t) = -K \begin{bmatrix} \theta \\ \dot{\theta} \\ x \\ \dot{x} \end{bmatrix}$$

typical closed response



measure
of performance $\int_0^{\infty} \theta^2(t) dt$



$\int_0^{\infty} \omega^2(t) dt$

choose the objective

(4)

$$J = q_1 \int_0^{\infty} \dot{\theta}^2(t) dt + q_2 \int_0^{\infty} \dot{\omega}^2(t) dt + q_3 \int_0^{\infty} \dot{x}^2(t) dt \\ + q_4 \int_0^{\infty} v^2(t) dt + r \int_0^{\infty} F^2(t) dt$$

Aside: q_i reflects the importance of $\int_0^{\infty} x_i^2(t) dt$ in the optimization

q_i is the penalty on x_i in J

$$J = \int_0^{\infty} \left(\begin{bmatrix} \dot{\theta} & \dot{\omega} & \dot{x} & v \end{bmatrix} \begin{bmatrix} q_1 & 0 & 0 & 0 \\ 0 & q_2 & 0 & 0 \\ 0 & 0 & q_3 & 0 \\ 0 & 0 & 0 & q_4 \end{bmatrix} \begin{bmatrix} \dot{\theta} \\ \dot{\omega} \\ \dot{x} \\ v \end{bmatrix} + F r F \right) dt$$

general form

$$\int_0^{\infty} (x^T Q x + u^T R u) dt$$

Terminology:

5

$$J = \int_0^{\infty} \underbrace{x^T Q x}_{\text{state regulation}} + \underbrace{u^T R u}_{\text{control effort}} dt$$

Typically: state regulation and control effort are competing objectives

LQR gives a systematic method to trade off regulation vs. control effort

Rule of thumb for picking weights
(Q, R are called the LQR weights)

$$J = \int_0^{\infty} \left(\frac{x}{x_{\max}} \right)^2 + \left(\frac{u}{u_{\max}} \right)^2 + \left(\frac{F}{F_{\max}} \right)^2 dt$$

these are called Bryson's Rules (6)

Q, R diagonal

$$q_i = \frac{1}{\text{max. allowable deviation in } x_i^2}$$

This is a rough guideline, not a precise mathematical constraint.

Example: 7.6 (DC servo)

states



$$J = \int_0^{\infty} (Q_{11} (\theta - \theta_d)^2 + Q_{22} \omega^2 + v^2) dt$$

$$= \int_0^{\infty} \begin{bmatrix} \dot{\theta} & \omega & v \end{bmatrix} \begin{bmatrix} Q_{11} & 0 & 0 \\ 0 & Q_{22} & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\theta} \\ \omega \\ v \end{bmatrix} dt$$

Design by using LQR for various values of Q_{11}, Q_{22}

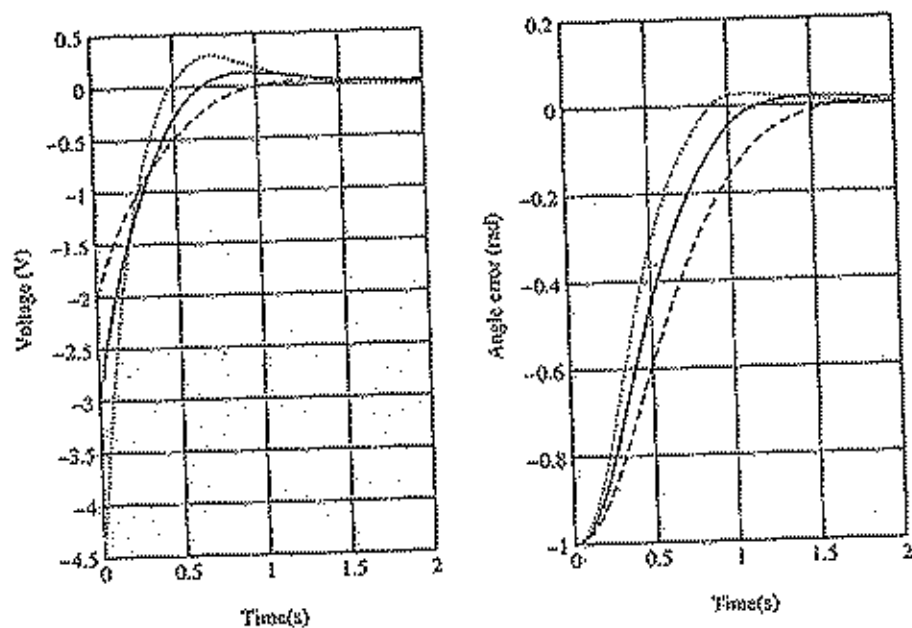


Figure 7.8 Results of LQ design for the dc servo: input voltage and angle error for $Q_{11} = 4$ (dashed), 9 (solid), and 20 (dotted)

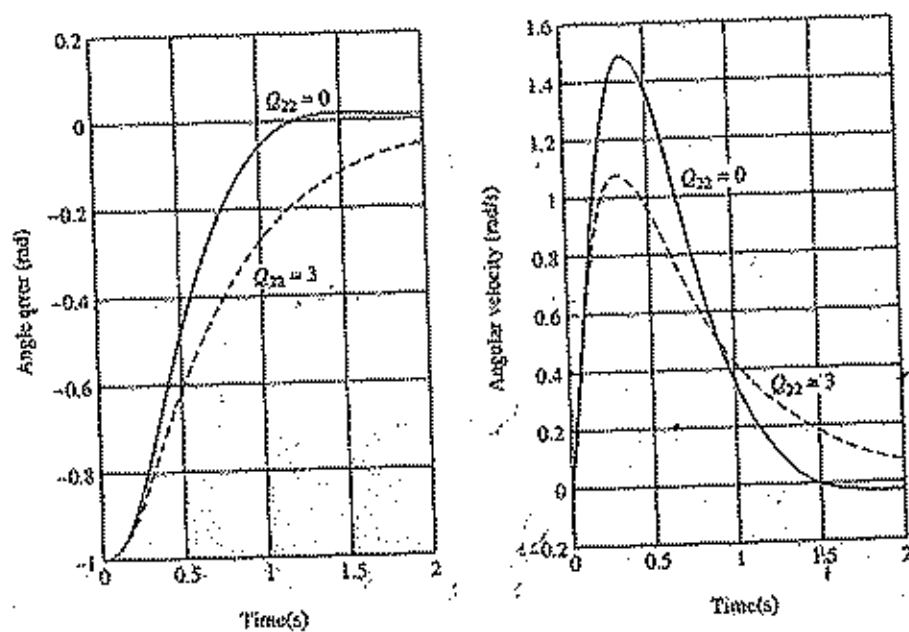


Figure 7.9 Results of LQ design for the dc servo: effect of weighting the angular velocity

Optimal Observers:

(8)

■ Observation model

$$\dot{x} = Ax + Bu + W$$

↑
process noise

$$y = Cx + V$$

↑
measurement noise



matrices V & W represent the variances of these noise processes

think diagonal V & W

the diagonal elements of V & W are

the variances of corresponding components of random vectors v & w

optimal observer design gives
a procedure to produce optimal
observer gain given

$$A, C, W, V \longrightarrow \text{optimal } L$$

(book calls L a G)

via solving Algebraic Riccati
Equation

(in matlab "care")